Physical Layer Simulation of Large Distributed Automation Systems in SPICE

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Abstract—In this paper, we propose an analysis of the physical layer of large distributed automation systems based on simulation in SPICE. For large systems, changes of the physical topology or minor modifications of the physical layer hardware of a bus node result in much more increased influences to the signal integrity compared to smaller system architectures. The simulation provides references for further designs of the physical layer hardware of a bus node and an analysis of its behavior in different large topology configurations with up to 1000 bus nodes in a network with a total length of up to 1000 meters.

Keywords- large distributed automation systems; physical layer simulation; signal integrity; fieldbus simulation

I. INTRODUCTION

Due to the increase in performance and the cost reduction of micro-processors, the decentralized approach of automation systems is used more and more in the last years. Furthermore, current developments of automation systems focus on distributed systems to handle modular extensibility and to avoid isolated applications. The decentralized approach suggests a connection of each sensor and actuator to a bus system via a bus coupler. As a result a large distributed automation system is generated, of which behavior is dependent on a high number of influence factors, based on the complex structure of the transmission channel system and the large number of bus participants.

Current research on physical layer simulations in works mainly in the field of automotive bus systems ([1]-[6]) or focused on lower scale case studies ([7], [8]). In this paper the focus lies on more complex bus system topologies, for example hardware architectures in decentralized building automation systems, which contain more than 1000 bus couplers which are networked in a transmission channel system of up to 1 km without a repeater. Changes of the physical topology or minor modifications of the physical layer hardware of a bus node, such as stub lines, mismatches or unsuitable dimensioning, could cause a negative influence to the signal integrity. A simulation based analysis is essential for this kind of large distributed automation systems.

Based on the fieldbus system SmallCAN ([9] and [10]), developed at the Institut for traffic safety and automation engineering, Technische Universität Braunschweig, the signal integrity for a large distributed automation system is validated by a physical layer simulation in SPICE.

Therefore, the main components models of the mentioned automation system and their connection to a large distributed system are described in section 2 of this paper.

In section 3 the main requirements for a sufficient signal integrity behavior in SmallCAN are introduced.

In section 4 the results are shown after simulation. Next to specific complex topology configurations with up to 1000 bus participants, the influence of modifications of the physical layer hardware of a bus node is also be analyzed.

II. Simulation model

To simulate the data transmission system for SmallCAN, three main components of the data transmission system are modeled in SPICE:

- energy supply unit.
- physical layer hardware of a bus coupler.
- transmission channel system.

The energy supply unit provides a recessive signal level of 24 V for the data line and a constant current source which impresses a current of 250 mA in case of a forced dominant signal level. The developed model ENERGY_SUPPLY_UNIT supports three ports for ground, input power supply and data line.

The dominant signal level is caused by short-circuiting the data line to the ground, executed by a MOSFET-Transistor of an active bus coupler. The developed model BUS_COUPLER represents a bus coupler with the logical input port for transmitting data, the data line of the bus, ground and the logical output port for the receiving data.

The transmission channel system of SmallCAN considers the electrical parameters for a typical phone cable:

- capacitance per unit C' = 55 $\frac{\text{pF}}{\text{m}}$. resistance per unit R' = 0,05 $\frac{\Omega}{m}$. inductance per unit L' = 0,075 $\frac{uH}{m}$.

For the transmission channel system the SPICE model TLUMP128 is used. The individual models of the components are connected to a whole system model of the specific hardware architecture, described by a SPICE net list. The physical topology can be chosen free, as long as the total cable length is lower than 1000 m.

Figure 1 shows a minimal topology with 3 bus couplers at a maximum distance of 3 *m* and the accordance net list. Two phone cables with 1 *m* and 2 *m* are connected between the energy supply unit X_Z1 and the bus couplers X_B2 and X_B3. A pulse, generated by the voltage source V_V3, controls the logical input port of bus coupler X_B3 to trigger the dominant signal level on the bus. The energy supply unit feeds in a current of 250 *mA* in the data line in the direction of the active bus coupler X_B3.



V_V3 EVENT GND_2 PULSE 0V 5V 1000u 10n 10n 0.1m 0.198m

Fig. 1. Minimal scale hardware architecture and SPICE-net list.

In Figure 2 an example of a maximal periodically structured topology with 991 bus couplers of a total cable length of 1 km and a section of its net lists are depicted. The energy supply unit X_Z1 is placed in the middle of the system, from where two main lines were extended. Each following stub line has a length of 20 m. At each end of the stub line a network, composed of 33 bus couplers, is located.

III. Requirements

After short-circuiting, the following signal curve depends on signal integrity properties, such as reflection behavior and voltage changes. The following requirements have to be fulfilled for each topology configuration to guarantee a sufficient signal integrity behavior:

- The voltage drop between the data line and the ground has to be lower than 7 V / 500 m, which guarantees the recognition of the dominant signal by the receiver hardware.
- After the settling time and line delay time of 11,9 us the level signal on the data line has to be lower than the threshold voltage of 14 V during the falling edge and has to be overrun it during the rising edge, to ensure a stable signal trace before the signal sampling starts.



- X_Z1
 0
 2
 1
 ENERGY_SUPPLY_UNIT

 X_B1
 XX_1
 2
 0
 20001
 BUS_COUPLER

 X_T1
 3
 2
 T1_0
 TLUMP128
 PARAMS: R=0.05 L=0.075u C=55p
 LEN=20
- X_T22 22 22 T23_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20 X_T23 24 23 T24_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20 X_B430 XX_430 24 T24_0 20430 BUS_COUPLER
- X_B462 XX_462 24 T24_0 20462 BUS_COUPLER X_T25 25 23 T25_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20 X_B463 XX_463 25 T25_0 20463 BUS_COUPLER
 - X_B495 XX_495 25 T25_0 20495 BUS_COUPLER
- X_T25 26 2 T26_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20
- ... X_T48 50 48 T48_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20 X_T49 51 50 T49_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20 X_B926 XX_926 51 T49_0 20926 BUS_COUPLER
- X_B958 XX_958 51 T49_0 20958 BUS_COUPLER X_T50 52 50 T50_0 TLUMP128 PARAMS: R=0.05 L=0.075u C=55p LEN=20 X_B959 XX_959 52 T50_0 20959 BUS_COUPLER ... X_B991 EVENT 52 T50_0 20991 BUS_COUPLER V_V3 EVENT T50_0 PULSE 0V 5V 1000u 10n 10n 0.1m 0.198m

Fig. 2. Large scale hardware architecture and section of the SPICE-net list.

IV. SIMULATION RESULTS

In Figure 3 (a),(b), the simulation results are depicted for the mentioned large distributed topology. For comparison an ideal trace for the minimal system with three bus couplers by a total cable length of 3 m is also depicted in Figure 3 (c),(d). The voltage between the data line and data ground is measured near the active bus coupler X_B991(cyan), near the energy supply unit at bus coupler X_B1 (red) and far from the active bus coupler at the bus coupler X_B495 (blue).

The simulation results show that the voltage drop between data line and ground is lower than the permitted value of 7 V. Due to the influence of the line capacity the signal trace results in a much flattened curve in contrast to the signal curve for the minimal system. It can be also seen that during the falling edge more signal levels are formed,



Fig. 3. Simulation results for a large and minimal distributed topology.

due to the reflection behavior. After a line delay time of nearly 2,5 us and the settling time the signal is fall below the threshold voltage of 14 V within the permitted time of 11,8 us.

The trace of the steep edges, affiliated under minimal topology conditions, cannot be kept for extended topology configurations, due to the resulting flattened curve. Furthermore, for smaller system topologies the steep edges result in excessive emitted interferences. Therefore, some modifications of the physical hardware of the bus coupler are implemented to avoid the steep edges during signal level changes. By a delayed triggering of the output transistor, the current flow in the data line is impressed under controlled conditions to avoid the steep edges.

In Figure 4, the simulation results after the hardware modifications of the transmitter are depicted. Due to the controlled triggering of the output transistor, the signal behavior for the large distributed topology resembles more the signal behavior for the minimal system, compared to the simulation results of Figure 3. The mentioned signal integrity requirements are fulfilled and the reflection behavior is reduced. In summary it could be assumed, that for different topology configurations the signal trace on the data line is more predictable after the mentioned hardware modifications.



Fig. 4. Simulation results for a large and minimal distributed topology after hardware modification.

V. CONCLUSION AND OUTLOOK

The effort for a measurement based analysis of the physical layer of large distributed automation systems is extremely high and not practical. Therefore, a simulation based analysis for this kind of automation systems is proposed in this contribution. The main component models of an automation system and theirs variable connection by a topology net are described. The simulation results for different case studies show various signal behaviors, dependent on different bus topologies and modifications of the transceiver hardware. Variable parameters allow the analysis of signal integrity for different conditions. Generally, statements about the signal integrity for complex automation systems can be yielded by this simulation.

In further works, an optimized signal behavior for all conditions could be found by an automated modification of parameters, simulation execution and an analysis of the results. Monte Carlo simulations, offered by SPICE Tools, could be used for that.

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